## FULTON COUNTY PUBLIC WORKS DEPARTMENT TRANSPORTATION PLANNING

## PROJECT CONCEPT REPORT Butner Road Bridge Replacement over Camp Creek

Fulton County Project Number: T227 County: FULTON COUNTY

May 28, 2010

Recommendation for approval:	
DATE	Angela Parker
DATE	Richard Coates Assistant Director of Public Works
DATE	Antonio Valenzuela County Transportation Planning Administrator

**Need and Purpose:** The existing bridge structure at Butner Road over Camp Creek has been inspected and evaluated by the Georgia Department Of Transportation and is listed in their Bridge Inventory Data listing dated October 20<sup>th</sup>, 2004. The bridge structure I.D. no. is 121-0355-0. The bridge was constructed in 1946 and is currently posted for 20 Tons load and opens to traffic. Currently, the existing narrow bridge has a sufficiency rating of 19, which is very low and requires immediate attention to maintain the traffic flow from Camp Creek Parkway across Camp Creek on Butner Road.

The primary purpose of the proposed project is to replace a deficient bridge at the crossing of Butner Road and the Camp Creek and to provide additional capacity along the corridor and to provide an efficient and safe movement of traffic that is consistent with the functional classification of a minor arterial as well as upgrades the bridge crossing to the accepted level of HS 20-44 of the AASHTO standards for bridges.

**Description of the proposed project:** A new bridge is proposed to replace the existing Butner Road Bridge near Camp Creek Parkway / Butner Road Intersection. The proposed bridge will be wide enough to accommodate four traffic lanes of 12ft wide and 24in curb and gutter and 12 feet wide pedestrian sidewalk on the west side to tie into the multi-use trail off the bridge and six foot sidewalk on the east side. There will be one SB traffic lane, one NB Left turn lane, one NB through traffic lane and one NB right turn lane. Both the left turn lane and the right turn lane will extend on to the proposed bridge to furnish free flow and stacking length up to the intersection with Camp Creek Parkway.

No intersection improvements at Camp Creek Parkway are included with this concept. Bridge and the roadway north of the bridge will be designed for a four lane section and roadway south of the bridge will be designed for a two lane section. Project must be let in conjunction with intersection work so as to allow a left turn lane from Butner Road to Camp Creek Parkway and line up the thru lanes. If an intersection project is not let concurrently with this project then the roadway would be striped for a two lane section.

The length of the bridge shall be approximately 90 ft for alternative #1, 130 ft for alternative #2, and 130 ft for alternative #3. The new bridge elevation will be raised depending on the HEC-RAS study but at minimum it will be maintained at about two feet above the elevation of the existing bridge. The approach road on each side of the bridge shall be widened to match the existing road approaching this bridge. The project begins approximately 1200 feet south of the Camp Creek Parkway intersection, and extends north along Butner Road to Camp Creek Parkway intersection. The logic behind the chosen termini is to ensure the highest level of service at the Camp Creek Parkway/ Butner road intersection. Please refer to location map attached.

Is the project located	l in a Non-attainment	t area? X	Yes No.	
PDP Classification:	Major Mino	or <u>X</u> _		
Federal Oversight:	Full Oversight ( ),	Exempt(X),	State Funded ( ),	or Other ( )

Functional Classification: <u>Urban M</u>	finor Arterial
Route Number(s):	State Route Number(s):
Traffic (AADT):	
Current Year: (2012) Traffic Data: CR 1374 - Butner Road over Camp C 2007 ADT: 5610 vpd 2012 ADT: 6300 vpd 2032 ADT: 9700 vpd 2032 DHV: 875 vph Directional Dist. = 55/45 24-hr T% = 5% SU = 3% and COMB T% = 4%	
<ul> <li>Posted speed45 _mph</li> <li>Maximum super-elevation rat</li> <li>Maximum grade:5</li></ul>	% (List mainline, cross roads, and driveways)
pedestrian sidewalks respective Proposed Design Speed Main Proposed Maximum grade Mae Proposed Maximum grade Side Proposed Maximum grade dried Proposed Minimum radius for Proposed Maximum super-electory Proposed Maximum degree of Right of way  Midth 100 FT  Easements: Temporary	line45_ mph ainline5_%; Maximum grade allowable5_%. de Street_NA_%; Maximum grade allowable_NA_%. iveway_NA_% r curve_NA_Maximum radius allowable_NA_

0	Number of parcels:	5	Nι	umber of displacements: NONE
			0	Business: X
			0	Residences: X.
			0	Mobile homes:
			0	Other:

### • Structure:

o Bridges: For all bridge alternatives, the bridge will be 72'-5" wide (Out-to-Out) that provides for four 12 ft travel lanes, One 12'-0" sidewalk on the west side and one 6'-0" sidewalk on the east side, two 24" curb & gutter, and two 1'-2½" parapets. End bents will be parallel and built at 90°-00'-00" to the Camp Creek centerline to align with the flood flow. The proposed PGL profile will be approximately 2.0 ft above the existing grade, measured as shown on the roadway profile. This proposed grade would provide for a minimum of 2 ft freeboard and a minimum clearance below the superstructure low chord for a 50-year flood stage design year per GDOT stipulations in the Manual for Hydrological crossings.

### Design Alternative 1. Single Span Type III Beam Bridge Structure

This proposed bridge alternative consists of a single span 90.0 ft long with vertical cast-in-place concrete abutments. The superstructure will consist of a standard 45 inch deep precast prestressed concrete Type III PSC beams supporting a cast in place concrete deck. The entire superstructure will be supported on two vertical cast-in-place abutments on pile with wingwalls. The face of the abutment wall to the face of the abutment wall length of the proposed bridge is  $90\pm$  ft. This alternative doesn't require any piers in the creek. The downside of this alternative is that the two abutments require pile foundations and a lot of cast-in place-concrete, thus making it the most expensive alternative.

### Design Alternative 2. Two Span PSC Beam Bridge Structure

This proposed bridge alternative is 130 ft long and consists of two 65 ft spans with spill through end bents. The superstructure will consist of standard AASHTO Type II (36 inch deep) precast prestressed concrete (PSC) beams supporting a cast in place concrete decks. The entire superstructure will be supported in the middle on one concrete intermediate bent on pile footings and at the end on two pile end bents. The toe of the endroll to toe of endroll length of the proposed bridge is  $100\pm$  ft. This alternative increases the channel opening under the bridge, so it works better hydraulically. The downside of this alternative is that it has a pier in the creek, thus requires cofferdams during construction and raises construction cost.

### Design Alternative 3. Single Span 130 ft Bulb Tee PSC Beam Bridge Structure

The proposed bridge consists of single span 130 ft long with spill through end bents. The superstructure will consist of standard Bulb Tee (65 inch deep) precast pre-stressed concrete (PSC) beams supporting a cast-in place concrete deck. The entire superstructure will be supported on two end bents on pile. The toe of the end-roll to toe of end-roll length of the proposed bridge is  $100\text{ft}\pm$ . This alternative is the most economical design because no costly concrete abutments and cofferdams are needed. This alternative also works better hydraulically than the other two alternatives.

For all three bridge alternatives see Concept Layouts and associated cost comparison.

### **Retaining walls**

- Retaining walls will be required in all four quadrants to avoid encroachment on the FEMA floodplain for this site. These retaining walls will range in height from 5'-20' and 50-100' feet long that run parallel to the shoulder lines.
- Major intersections and interchanges. <u>BUTNER ROAD/CAMP CREEK PKWY</u> INTERSECTION
- Traffic control during construction: <u>Traffic will be detoured from the existing bridge</u> while the new bridge is being built on the existing bridge location
- Design Exceptions to controlling criteria anticipated:

	<u>UNDETERMINED</u>	<u>YES</u>	NO
HORIZONTAL ALIGNMENT:	()	()	(x)
ROADWAY WIDTH:	()	()	(x)
SHOULDER WIDTH:	()	()	(x)
VERTICAL GRADES:	()	()	(x)
CROSS SLOPES:	()	()	(x)
STOPPING SIGHT DISTANCE:	()	()	(x)
SUPERELEVATION RATES:	()	()	(x)
HORIZONTAL CLEARANCE:	()	()	(x)
SPEED DESIGN:	()	()	(x)
VERTICAL CLEARANCE:	()	()	(x)
BRIDGE WIDTH:	()	()	(x)
BRIDGE STRUCTURAL CAPACIT	Y: ()	()	(x)

- Design Variances; N/A
- Environmental concerns: Wetland Section 404 Permit
- Level of environmental analysis:
  - o Are Time Savings Procedures appropriate? Yes (), No (),
  - o Categorical exclusion (),
  - o Environmental Assessment/Finding of No Significant Impact (FONSI) ( ), or
  - o Environmental Impact Statement (EIS) ( ).
- Utility involvements:
  - o Graystone Power Corporation
  - o Bellsouth Transportation Improvement Group

- o City of Atlanta Depart. of Watershed Management
- Colonial Pipeline Company
- o Plantation Pipeline Company

### **Project responsibilities:**

Design: FTC, Inc.
 Right of Way Acquisition: FTC, Inc.
 Relocation of Utilities: FTC, Inc.
 Letting to contract: Fulton County
 Supervision of construction: Fulton County
 Providing material pits: Contractor
 Providing detours: Contractor

### Coordination

- Initial Concept Meeting date and brief summary- Attach minutes.
- Concept meeting date and brief summary- Attach minutes.
- FEMA *No rise certificate*
- Public involvement *PIOH*
- Local government comments. See attached minutes of meeting with C.O.A.
- Other projects in the area. *None*
- Railroads N/A

### **Scheduling – Responsible Parties' Estimate**

- Time to complete the environmental process: 2 Months.
- Time to complete preliminary construction plans: <u>3</u> Months.
- Time to complete right of way plans: <u>6</u> Months.
- Time to complete the Section 404 Permit: 6 Months.
- Time to complete final construction plans: <u>8</u> Months.
- Time to complete to purchase right of way: <u>6</u> Months.
- List other major items that will affect the project schedule: <u>2</u> Months.

**Other alternates considered**: (Describe in summary and coordinate with environmental. If rejected ensure environmental is in agreement).

**Comments:** *As appropriate* 

### **Roadway Cost Estimates:**

1	Estimated Construction Cost (Roadway)	\$1,076,342.35
2	E & C Rate @10%,	\$107,634.53

3	Inflation 2% @ 1Year	\$23,679.53
4	Right-of-way	\$40,000.00
5	Reimbursable Utilities	\$0.00
	Sub-total (Roadway)	\$1,247,656.12

### **Bridge Cost Estimate:**

Alternative 1: \$1,493,188.00 Alternative 2: \$1,362,662.00 Alternative 3: \$1,250,233.00

### **Total Cost Estimate (Roadway plus Bridge):**

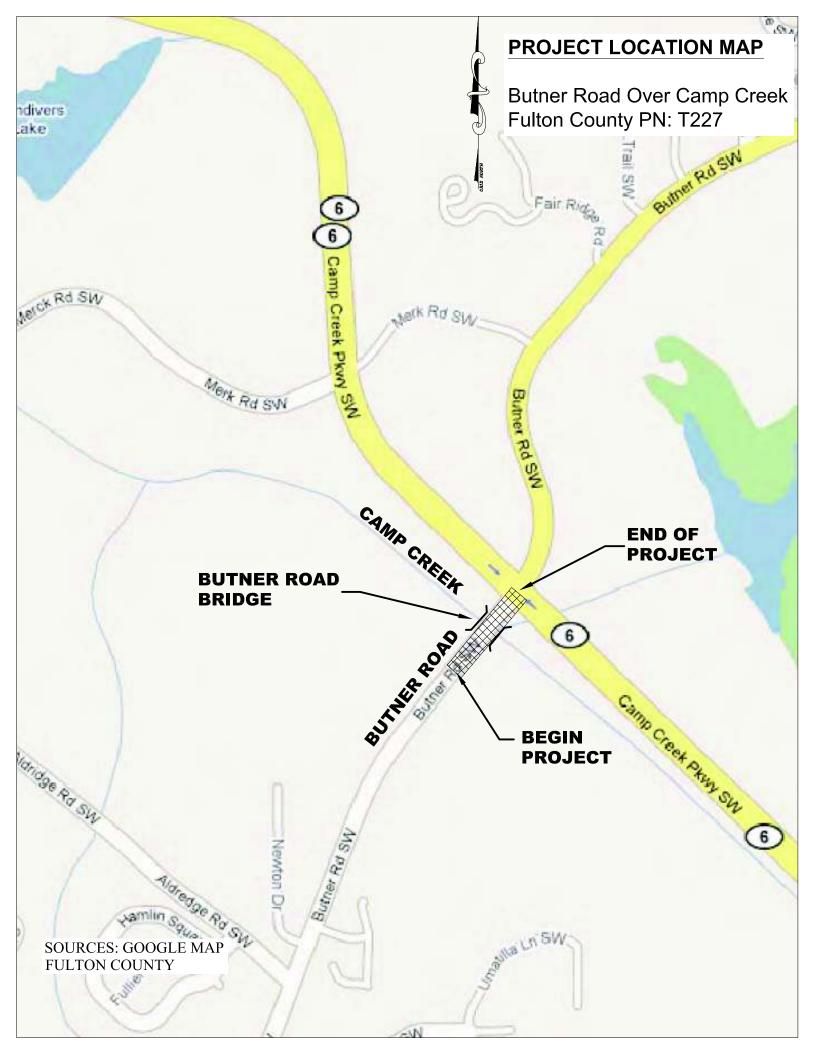
Alternative 1: \$1,493,188.00 + \$1,247,656.12= \$2,740,844.12

Alternative 2: \$1,362,662.00 + \$1,247,656.12= \$2,610,318.12

Alternative 3: \$1,250,233.00 + \$1,247,656.12= \$2,497,889.12

### **Attachments:**

- 1. Sketch location map
- 2. Traffic Analysis
- 3. Hydraulic Design Considerations
- 4. Typical Sections
- 5. Concept Road Layout Plan and Profile
- 6. Roadway Construction Cost Estimate
- 7. Bridge Design Alternatives and Bridge Construction Cost Estimate
- 8. Bridge Inventory Data
- 9. Fulton County / City of Atlanta Construction Cost Division
- 10. Minutes of Meeting



### TRAFFIC ANALYSIS OF QUEUE LENGTH

The year 2009 traffic volumes were used to calculate the required storage length necessary for right turning traffic on Butner Road. The queue length of the turning movements and through traffic was calculated using the following procedures:

Storage Length (feet)	= % Effective x red	turning volume	•		unit conversion	X	headway factor	X	length of vehicle
Storag	ge Length =	queue	e length in	feet					

% of cycle length when turning movement has "red" indication % Effective red

Traffic Volume right turn volume 110 seconds Cycle Length

Unit Conversion 1 hour/3600 seconds

Headway Factor = 1.5 Length of Vehicle 20 feet

### Northbound Butner Road at Camp Creek Pkwy

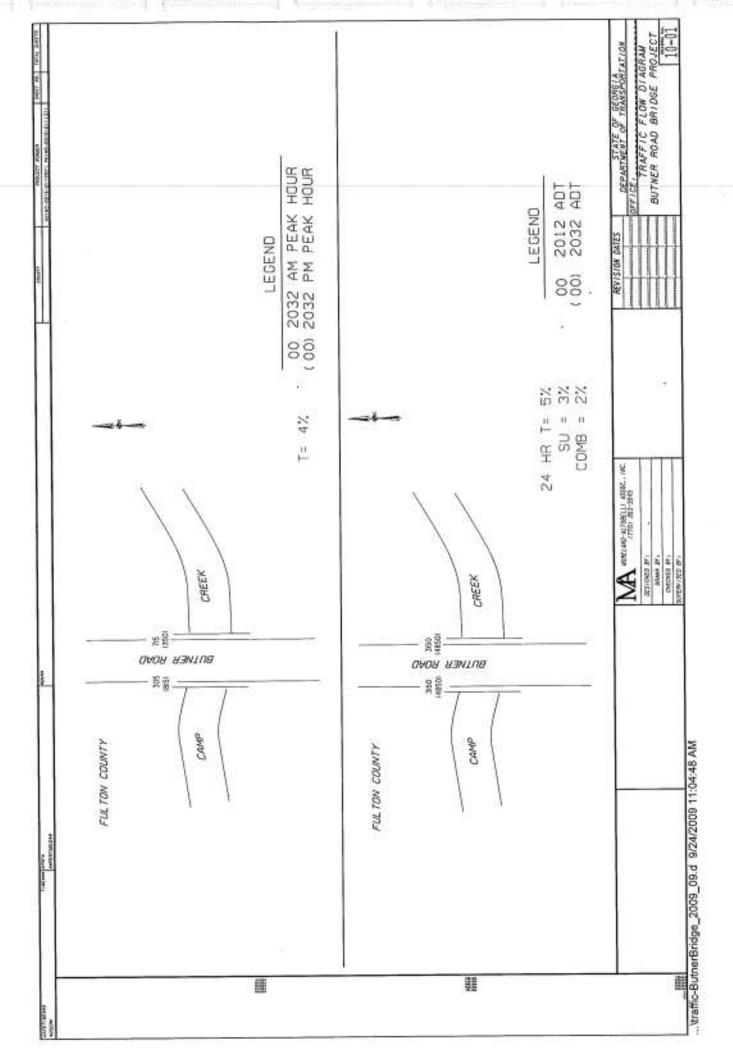
NB Right Turn	= 0.65	x 193	X	110	X	1/3600	X	1.5	X	20
Queue Length	=	115 feet								
<b></b>										
Two Alternatives:										
1) NB Left/Thru l	Lane =	$0.65  ext{ x}$	254	X	110	x 1/3600	X	1.5	X	20
Queue Length										
C										
2) NB Right/Thru	ı Lane =	0.65 x	227	' x	110	x 1/3600	X	1.5	x	20
Queue Length		135 feet	- <b>-</b> ,		-10					
Queue Lengin	_	133 1661								

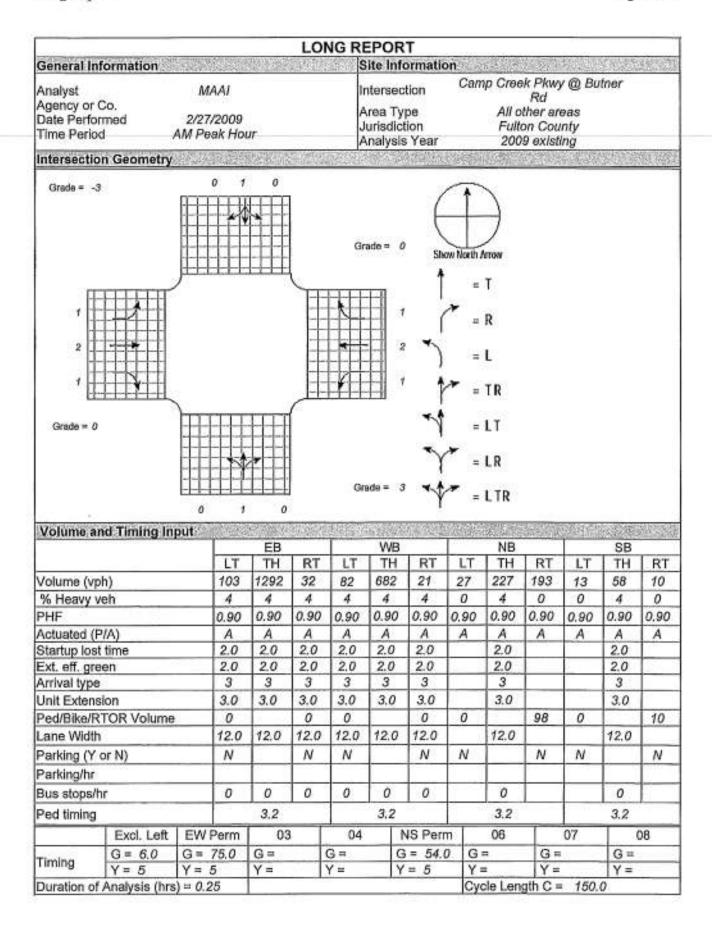
In case 1, the northbound right turn bay needs to be at least 151 feet in length so that it will not be blocked by the through traffic lane in the case where thru and left turn traffic share a lane.

In case 2, the northbound right turn bay will need to be 135 feet in length so that it will not be blocked by the through traffic lane.

Additionally in case 2, a sufficient length of left turn lane should be provided to store the proposed vehicular turning traffic. For 45 vehicles that distance is 50 feet.

It is recommended that the 100-foot taper begin at the end of the bridge and that a 12-foot right turn lane be constructed from the taper to the intersection. This will provide  $180 \pm \text{feet}$  of right-turn storage.





General Inform	ation	<b>医眼觉</b> 深		50 Jan 19		7.16			THE WAY			
Project Description	Secretaria de la constantina della constantina d	Road Bi	ridge Re	placem								
Volume Adjusti	ment	A CONTRACTOR									2866	
18 A 04 C 20 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A		EB			WB			NB			SB	
	LT	TH	RT	LT	TH	RT	LT	TH	RT	LT	TH	RT
Volume	103	1292	32	82	682	21	27	227	193	13	58	10
PHF	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Adj. Flow Rate	114	1436	36	91	758	23	30	252	106	14	64	0
Lane Group	L	T	R	L	T	R		LTR			LTR	
Adj. flow rate	114	1436	36	91	758	23		388			78	
Prop. LT or RT	0.000	-	0.000	0.000		0.000	0.077		0.273	0.179		0.000
Saturation Flov	v Rate	1000										
Base satflow	1900	1900	1900	1900	1900	1900		1900	III.SS.ZSCHI		1900	
Num. of lanes	1	2	1	1	2	1	0	1	0	0	1	0
fvv	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1,000	
fHV	0.962	0,962	0.962	0.962	0.962	0.962		0.975			0.968	
fg	1.000	1.000	1.000	1.000	1,000	1.000		0.985			1.015	
fp	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	
fbb	1.000	1.000	1,000	1.000	1.000	1.000		1.000			1.000	
fa	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
fLU	1.00	0.95	1.00	1.00	0.95	1.00		1.00			1.00	
fLT	0.950	1.000		0.950	1.000	***		0.973	44		0.912	-
Secondary fLT	0.267			0.059								-
fRT		1.000	0.850	-	1,000	0.850	-	0.963		-	1.000	1
fLpb	1.000	1.000		1.000	1.000	-		1.000	-		1.000	
fRpb	-	1.000	1.000	==	1.000	1.000	-	1.000		-	1.000	
Adj. satflow	1736	3471	1553	1736	3471	1553		1710			1703	
Sec. adj. satflow	488			109		-			-			

		CAPA	CITY A	AND L	os wo	RKSHE	ET					
General Information	on						fire of the rail					
Project Description B	utner Road	Bridge	Replace	ement P	roject							
Capacity Analysis						124						
		NB	SB									
Lane group	L	T	R	L	T	R	LTR	LTR				
Adj. flow rate	114	1436	36	91	758	23	388	78				
Satflow rate	1736	3471	1553	1736	3471	1553	1710	1703				
Lost time	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0				
Green ratio	0.57	0.50	0.50	0.57	0.50	0.50	0.36	0.36				
Lane group cap.	329	1736	777	127	1736	777	616	613				
v/c ratio	0.35	0.83	0.05	0.72	0.44	0.03	0.63	0.13				
Flow ratio	11/13	0.41	0.02		0.22	0.01	0.23	0.05				
Crit. lane group	N	Y	N	N	N	N	Y	N				
Sum flow ratios	4					0.68						
Lost time/cycle						15.00						
Critical v/c ratio	o sepuration		000000	n en en		0.76						
Lane Group Capa	city, Con	trol De	elay, a	nd LO	S Dete	rminatic	in .	ing Parallel Section				
		EB			WB		NB	SB				
Lane group	L	T	R	L	T	R	LTR	LTR				
Adj. flow rate	114	1436	36	91	758	23	388	78				
Lane group cap.	329	1736	777	127	1736	777	616	613				
v/c ratio	0.35	0.83	0.05	0.72	0.44	0.03	0.63	0.13				
Green ratio	0.57	0.50	0.50	0.57	0.50	0.50	0,36	0.36				
Unif. delay d1	16.4	32.0	19.2	27.8	24.0	19.0	39.7	32.2				
Delay factor k	0.11	0.37	0.11	0.28	0.11	0.11	0.21	0.11				
Increm. delay d2	0.6	3.5	0.0	17.6	0.2	0.0	2.1	0.1				
PF factor	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000				
Control delay	17.1	35.4	19.2	45.4	24.2	19.0	41.8	32.3				
Lane group LOS	В	D	В	D	С	В	D	С				
Apprch. delay	3	33.8 26.2 41.8 32.3										
Approach LOS		С		1	С	*	D	С				
Intersec. delay	3.	2,5	32,5 Intersection LOS C									

SUPPLEMENTAL L						T TURNS FROM D PHASES	EXCLUSIVE	
General Information	on							
Project Description B	utner l	Road Bridge	Replacemen	t Project				
v/c Ratio Computa	ation					0.24		
ECOLO COLORADO EL COLOR DE DESCRIPTO			EB	W	/B	NB	SB	
Cycle length, C (s)					150	0.0		
Prot. phase eff. green i	ntvl, g	(s)	6.0	6.	0			
Opposed queue eff. gre	en int	vl, gq (s)	21.36	54.	28			
Unopposed green intvl,	gu (s)		58.64	25.	72			
Red time, r(s)			64.0	64	.0			
Arrival rate, qa (veh/s)			0.03	0.0	03			
Prot. phase departure r	ate, sp	(veh/s)	0.482 0.4		82			
Perm, phase departure	rate, s	ss (veh/s)	0.18	0.0	9			
Xperm			0.23 0		33			
Xprot (N/A for lagging le	eft-turn	is)	0.77 0.6		31			
Uniform Queue Size a	nd De	lay Comput	ations		121			
Queue at start of green	arrow	, Qa	2.03	1.6	32			
Queue at start of unsat	urated	green, Qu	0.68	1.3	37			
Residual queue, Qr			0.00	0.0	00			
Uniform delay, d1			16.4	27	.8			
Uniform Queue Size a	nd De	lay Equatio	ns		1			
	Case	Qa	Qu	Qr		d1		
If Xperm <= 1.0 & Xprot <= 1.0	1	qar	qagq	0	[0.5/(qaC)][rQa + Qa <sup>2(Sp - Qa)</sup> +gq Qa)		+gqQu + Qu <sup>2((S<sub>8</sub> -</sup>	
If Xperm <= 1.0 & Xprot > 1.0			Qr+ qagq	Qa - g(Sp - qa)	[0.5/(qaC)][rQa + g(Qa + Qr)+gq (Qr + Qu) + Qu2n9a - Qa)			
If Xperm > 1.0 & Xprot <= 1.0			qagq	Qu - gu(Ss - qa)	$[0.5/(q_aC)][g_qQ_u + g_u(Q_a + Q_r) + \Gamma(Q_r + Q_a) + Q_a^2\eta S_p - Q_{a0}$			
If X <sub>perm</sub> <= 1.0 (lagging lefts)	4	0	qa(r + gq)	0	[0.5/(qaC	[0.5/(qaC)][r + gq)Qu + Qu <sup>2/(Sa - Qa)</sup>		

 $q_a(r + g_q)$ 

0

q<sub>e0</sub>

Qu - gu(Ss -Qa)

If Xperm > 1.0 (lagging lefts)

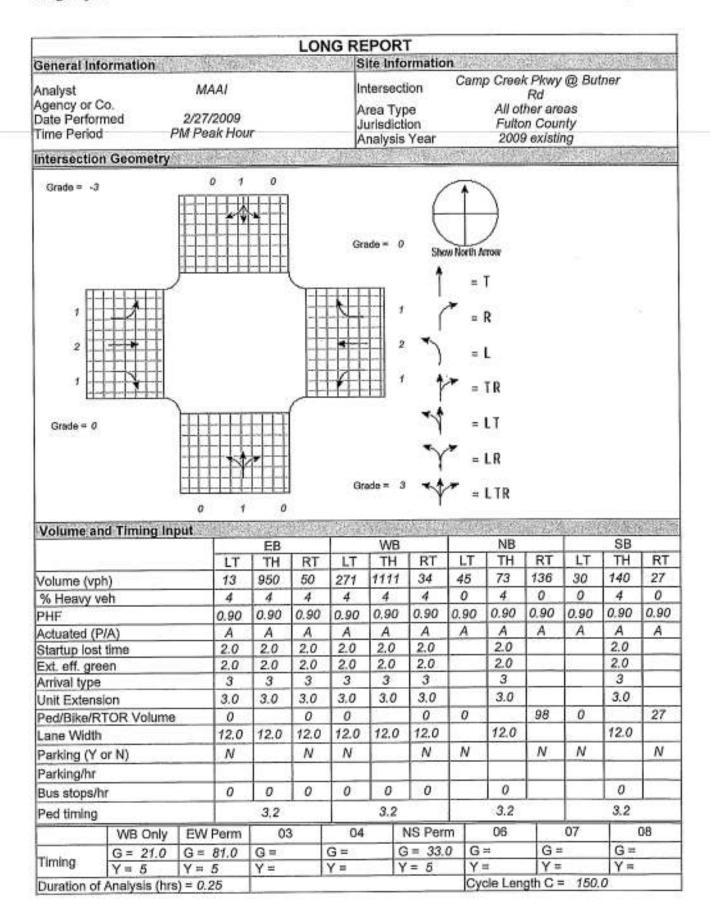
 $[0.5/(q_aC)][\Gamma + g_q)Q_u + g_u(Q_u + Q_a) + Q_a^{2i/S_p}$ 

	E	BACK-	OF-Q	UEUE	WOR	KSHE	ET					
General Informatio	n	0)07			10000				9	10 to 10		ile.
Project Description Bu	itner Road Bi	idge Re	placem	ent Pro	ject							
Average Back of Q	ueue				120							
	LT	TH	RT	LT	TH	RT	LT	NB TH	RT	LT	SB	RT
Lane group	L	T	R	L	T	R		LTR	101		LTR	181
Init. queue/lane	0.0	0.0	0.0	0.0	0.0	0.0		0.0			0.0	
Flow rate/lane	114	1436	36	91	758	23		388			78	
Satflow per lane	575	1826	1553	223	1826	1553		1710		î	1703	
Capacity/lane	329	1736	777	127	1736	777		616			613	
Flow ratio	0.20	0.41	0.02	0.41	0.22	0.01		0.23			0.05	
v/c ratio	0,35	0.83	0.05	0.72	0.44	0.03		0.63			0.13	
l factor	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	-
Arrival type	3	3	3	3	3	3		3			3	
Platoon ratio	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
PF factor	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
Q1	2.1	26.8	0.8	1.7	10.6	0,5		13.4			2.2	
kв	0.5	0.9	0.8	0.3	0.9	0.8		0.7			0.7	
Q2	0.3	3.6	0.0	0.6	0.7	0.0		1.1			0.1	
Q avg.	2.3	30.4	0.8	2.3	11.3	0.5		14.5			2.3	
Percentile Back of	Queue (95	th pe	rcentil	e)								
fB%	2.0	1.6	2.1	2.0	1.8	2.1		1.8			2.0	
BOQ, Q%	4.7	49.0	1.7	4.6	20,5	1.1		25.7			4.6	
Queue Storage Rat	tio			Value 1						15 31		
Q spacing	25.0	25.0	25.0	25.0	25.0	25.0		25.0			25.0	
Q storage	0	0	0	0	0	0		75			0	
Avg. Ro								4.8				
95% Ro%								8.6				

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Project Description	The second second	STREET, STREET	PER STATE OF THE PERSON NAMED IN	Harris and Control	AVENUE AND	Avenue von		(3.850) <u>V</u>		ON COTOR	表示的语	
Volume Adjustr	nent	EB		NAME OF TAXABLE PARTY.	WB		1000	NB	NEW CONTRACTOR	SHOWEN	SB	Manager S.
	LT	ТН	RT	LT	TH	RT	LT	тн	RT	LT	тн	RT
Volume	13	950	50	271	1111	34	45	73	136	30	140	27
PHF	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Adj. Flow Rate	14	1056	56	301	1234	38	50	81	42	33	156	0
Lane Group	L	т	R	L	т	R		LTR			LTR	
Adj. flow rate	14	1056	56	301	1234	38		173	ń –		189	
Prop. LT or RT	0.000	-	0.000	0.000		0.000	0.289		0.243	0.175	-	0.000
Saturation Flow	Rate										7,5	574.08
Base satflow	1900	1900	1900	1900	1900	1900		1900			1900	
Num. of lanes	1	2	1	1	2	1	0	1	0	0	1	0
rw	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	
fHV	0.962	0.962	0.962	0.962	0.962	0.962		0.982			0.968	
fg	1.000	1.000	1.000	1.000	1.000	1.000		0.985			1.015	
fp	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	
fbb	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	
fa	1.00	1.00	1.00	1.00	1,00	1.00		1.00			1.00	
fLU	1.00	0.95	1.00	1.00	0.95	1.00		1.00			1.00	
fLT	0.132	1.000		0.950	1.000			0.776			0.908	
Secondary fLT			-	0.174					-			**
fRT	-	1.000	0.850	-	1.000	0.850	85_	0.967		***	1.000	
fLpb	1.000	1,000		1.000	1.000			1.000	-		1.000	
fRpb	-	1.000	1.000		1.000	1.000		1.000	(		1.000	
Adj. satflow	241	3471	1553	1736	3471	1553		1380	1		1695	
Sec. adj. satflow				318					-			

General Informati		CONTRACTOR OF THE PARTY OF THE	ASSESSED TO	DE SAL	17. E. S.	ORKSHE	STEELS STREET	A CONTRACTOR OF THE PARTY OF TH
Project Description		Deleton	Donloo	oment C	rainet	C25507901E-VI2	SALE REPORT OF SHIP	ACTIVITY AND ADDRESS OF THE PARTY OF THE PAR
	and the second second	Briage	replaci	and the last section of the last section is	rojeci	200000000000000000000000000000000000000	TO THE PERSON NAMED OF THE	
Capacity Analysis	5	EB	SPERM		WB		NB	SB
1	L	T	R	L	T	R	LTR	LTR
Lane group Adj. flow rate	14	1056	56	301	1234	38	173	189
Satflow rate	241	3471	1553	1736	3471	1553	1380	1695
Lost time	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0
Green ratio	0.54	0.54	0.54	0.71	0.54	0.54	0.22	0.22
Lane group cap.	130	1874	839	425	1874	839	304	373
v/c ratio	0.11	0.56	0.07	0.71	0.66	0.05	0.57	0.51
Flow ratio	0.06	0.30	0.04		0.36	0.02	0.13	0.11
Crit. lane group	N	N	N	N	Y	N	Y	N
Sum flow ratios		is .				0.62	10/2	FU 10 50
Lost time/cycle						15.00		
Critical v/c ratio					1000	0.69		
The second secon	10 Sept. 10				and a commence of the second section of the			
Lane Group Capa	city, Con	trol D	elay, a	nd LO	S Dete	rminatio	n a de la	
	city, Con	trol Do	elay, a	nd LO	S Dete	rminatio	n NB	SB
	city, Con		elay, a	nd LO		erminatio		The state of the s
Lane Group Capa	-20-10-10-	EB	-		WB		NB	SB
Lane Group Capa Lane group	. L	EB T	R	L	WB T	R	NB LTR	SB LTR
Lane Group Capa Lane group Adj. flow rate Lane group cap.	. L	EB T 1056	R 56	L 301	WB T 1234	R 38	NB LTR 173	SB LTR 189
Lane Group Capa Lane group Adj. flow rate	. L 14 130	EB T 1056 1874	R 56 839	L 301 425	WB T 1234 1874	R 38 839	NB LTR 173 304	SB LTR 189 373
Lane Group Capa Lane group Adj. flow rate Lane group cap. v/c ratio Green ratio	14 130 0.11	EB T 1056 1874 0.56	R 56 839 0.07	L 301 425 0.71	WB T 1234 1874 0.66	R 38 839 0.05	NB LTR 173 304 0.57	SB LTR 189 373 0.51
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1	. L 14 130 0.11 0.54	EB T 1056 1874 0.56 0.54	R 56 839 0.07 0.54	L 301 425 0.71 0.71	WB T 1234 1874 0.66 0.54	R 38 839 0.05 0.54	NB LTR 173 304 0.57 0.22	SB LTR 189 373 0.51 0.22
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k	. L 14 130 0.11 0.54 16.8	EB T 1056 1874 0.56 0.54 22.8	R 56 839 0.07 0.54 16.5	L 301 425 0.71 0.71 15.5	WB T 1234 1874 0.66 0.54 24.6	R 38 839 0.05 0.54 16.3	NB LTR 173 304 0.57 0.22 52.2	SB LTR 189 373 0.51 0.22 51.4
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k  Increm. delay d2	. L 14 130 0.11 0.54 16.8 0.11	EB T 1056 1874 0.56 0.54 22.8 0.16	R 56 839 0.07 0.54 16.5	L 301 425 0.71 0.71 15.5 0.27	WB T 1234 1874 0.66 0.54 24.6 0.23	R 38 839 0.05 0.54 16.3 0.11	NB  LTR  173  304  0.57  0.22  52.2  0.16	SB LTR 189 373 0.51 0.22 51.4 0.12
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k  Increm. delay d2  PF factor	. L 14 130 0.11 0.54 16.8 0.11	EB T 1056 1874 0.56 0.54 22.8 0.16 0.4	R 56 839 0.07 0.54 16.5 0.11	L 301 425 0.71 0.71 15.5 0.27 5.4	WB T 1234 1874 0.66 0.54 24.6 0.23 0.9	R 38 839 0.05 0.54 16.3 0.11	NB  LTR  173  304  0.57  0.22  52.2  0.16  2.5	SB LTR 189 373 0.51 0.22 51.4 0.12 1.1
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k  Increm. delay d2  PF factor  Control delay	. L 14 130 0.11 0.54 16.8 0.11 0.4 1.000	EB T 1056 1874 0.56 0.54 22.8 0.16 0.4 1.000	R 56 839 0.07 0.54 16.5 0.11 0.0 1.000	L 301 425 0.71 0.71 15.5 0.27 5.4 1.000	WB T 1234 1874 0.66 0.54 24.6 0.23 0.9 1.000	R 38 839 0.05 0.54 16.3 0.11 0.0 1.000	NB  LTR  173  304  0.57  0.22  52.2  0.16  2.5  1.000	SB LTR 189 373 0.51 0.22 51.4 0.12 1.1 1.000
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k  Increm. delay d2  PF factor  Control delay  Lane group LOS	. L 14 130 0.11 0.54 16.8 0.11 0.4 1.000 17.2 B	EB T 1056 1874 0.56 0.54 22.8 0.16 0.4 1.000 23.2	R 56 839 0.07 0.54 16.5 0.11 0.0 1.000 16.5	L 301 425 0.71 0.71 15.5 0.27 5.4 1.000 20.9 C	WB T 1234 1874 0.66 0.54 24.6 0.23 0.9 1.000 25.5	R 38 839 0.05 0.54 16.3 0.11 0.0 1.000 16.3	NB  LTR  173  304  0.57  0.22  52.2  0.16  2.5  1.000  54.7	SB LTR 189 373 0.51 0.22 51.4 0.12 1.1 1.000 52.5
Lane Group Capa  Lane group  Adj. flow rate  Lane group cap.  v/c ratio  Green ratio  Unif. delay d1  Delay factor k  Increm. delay d2  PF factor  Control delay	. L 14 130 0.11 0.54 16.8 0.11 0.4 1.000 17.2 B	EB T 1056 1874 0.56 0.54 22.8 0.16 0.4 1.000 23.2 C	R 56 839 0.07 0.54 16.5 0.11 0.0 1.000 16.5	L 301 425 0.71 0.71 15.5 0.27 5.4 1.000 20.9 C	WB T 1234 1874 0.66 0.54 24.6 0.23 0.9 1.000 25.5 C	R 38 839 0.05 0.54 16.3 0.11 0.0 1.000 16.3	NB  LTR  173  304  0.57  0.22  52.2  0.16  2.5  1.000  54.7  D	SB LTR 189 373 0.51 0.22 51.4 0.12 1.1 1.000 52.5 D

### SUPPLEMENTAL UNIFORM DELAY WORKSHEET FOR LEFT TURNS FROM EXCLUSIVE LANES WITH PROTECTED AND PERMITTED PHASES

General Information	on						
Project Description B	utner	Road Bridge	Replacemen	t Project			
v/c Ratio Computa	ation	The beautiful					1.7
			EB	V	VB	NB	SB
Cycle length, C (s)					150.	0	
Prot. phase eff. green i	ntvi, g	(s)		21	1.0		
Opposed queue eff, gre	en in	tvl, gq (s)		30.	.82		
Unopposed green intvl,	gu (s	)		55	.18		
Red time, r(s)				43	3.0		1,450.7
Arrival rate, qa (veh/s)			0.	08			
Prot. phase departure r	ate, s	(veh/s)		0.4	182		
Perm. phase departure	rate,	ss (veh/s)		0.	14		
Xperm				0.	95		
Xprot (N/A for lagging le	eft-turn	18)	10110150-0000	0.	53		
Uniform Queue Size a	nd De	lay Comput	ations				
Queue at start of green	arrov	/, Qa		3.	60		
Queue at start of unsat	urated	green, Qu		2.	58		
Residual queue, Qr				. O.	00		
Uniform delay, d1				15	5.5		
Uniform Queue Size a	nd De	lay Equation	ns		Company of the last	ARGO BAKA	
	Case	Qa	Qu	Qr		dı	
If Xperm <= 1.0 & Xprot <= 1.0	1	qer	qegq	0	[0.5/(qaC)] q <sub>a)</sub>	i) +gqQu + Qu <sup>2(5</sup> s -	
If Xporm <= 1.0 & Xprot > 1.0			Qr+ qugq	Qa - g(Sp - Qa)	[0.5/(qaC)] Qu <sup>2</sup> (S <sub>8</sub> - Q <sub>n</sub> )	r) +gq (Qr + Qu) +	
Xperm > 1.0 & Xprot 3 Qr + qaΓ		Qr+qar	qagq	Qu - gu(Ss - Qa)			
lf X <sub>perm</sub> <≔ 1.0 (lagging lefts)	= 1.0 (lagging 4 0		qa(r + gq)	0	[0.5/(QaC)][r + gq)Qu + Qu <sup>2</sup> /(S <sub>8</sub> - Q <sub>6</sub> )		
f Xperm > 1.0 (lagging 5 Qu - gu(Ss - qa)		Qu - gu(Ss - qa)	qa(r + gq)	0	$[0.5/(q_aC)][r + g_q)Q_u + g_0(Q_u + Q_a) + Q_a^{2/4}$ $q_a$		

	E	BACK	OF-Q	UEUE	WOR	KSHE	ET					
General Information	on		100				100		t de la companya de l			177
Project Description B	lutner Road Br	idge Re	placen	ent Pro	ject							
Average Back of 0	Queue									1910	10.00	
in a passacratic continuous in a continuous in	17	EB	RT	LT	TH	RT	NB			SB LT TH R		
Lane group	LT L	7	R	L	T	R	LT	TH LTR	RT	LI	LTR	RT
Init. queue/lane	0.0	0.0	0.0	0.0	0.0	0.0		0.0			0.0	
Flow rate/lane	14	1056	56	301	1234	38		173			189	
Satflow per lane	241	1826	1553	596	1826	1553		1380			1695	Н
Capacity/lane	130	1874	839	425	1874	839		304			373	
Flow ratio	0.06	0.30	0.04	0.51	0.36	0.02		0.13			0.11	
v/c ratio	0.11	0.56	0.07	0.71	0.66	0.05		0.57			0.51	
I factor	1.000	1.000	1.000	1.000	1.000	1.000		1.000			1.000	
Arrival type	3	3	3	3	3	3		3			3	
Platoon ratio	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
PF factor	1.00	1.00	1.00	1.00	1.00	1.00		1.00			1.00	
Q1	0.3	15.3	1.1	4.0	19.3	0.7		6.4			6.9	
kв	0.3	0.9	0.8	0.6	0.9	0.8		0.5			0.5	
Q2	0.0	1.2	0.1	1.3	1.7	0.0		0.6			0.5	
Q avg.	0.3	16.5	1.2	5.3	21.0	0.8		7.0			7.4	
Percentile Back o	f Queue (95	th pe	rcenti	e)				1000				
f8%	2.1	1.7	2.1	1.9	1.7	2.1		1.9			1.9	
BOQ, Q%	0.7	28.6	2.4	10.2	35.5	1.6		13.4			14.1	
Queue Storage Ra	itio	25,04				2						to N
Q spacing	25.0	25.0	25.0	25.0	25.0	25.0		25.0	147		25.0	
Q storage	0	0	0	0	0	0		75	-3-		0	
Avg. Ra								2.3				
95% Ra%								4.5				

### **Hydraulic Design Considerations**

The proposed project site is located in Fulton County which participates in the Federal Emergency Management Agency's (FEMA) National Flood Insurance Program (NFIP). The Community Flood Insurance Rate Map (FIRM) effective date is June 22, 1998 (Fulton County, FIRM Map Number 13121C0341 E, effective date June 22, 1998).

The proposed bridge is located in a designated flood zone AE, with base flood elevations (BFEs) and regulatory floodway established for this reach of Camp Creek. The effect of the proposed bridge and all the work necessary to address FEMA-related issues are the subject of a separate study, which is presented on a separate report.

Comparison of the results from the simulations using the existing conditions model and the proposed conditions model shows that the proposed conditions would not create an increase in the BFEs, floodway WSELs and floodway widths at any cross section outside of the County's right of way.

In conclusion, the results from the analysis are such that a "No-Rise" Certification can be issued for this reach of Camp Creek. Coordination with FEMA is not required but coordination with Community is required.

We have considered three (3) alternative bridge layouts to accommodate the roadway design.

Alternative I, is a 90-ft long span, made of 54" bulb-tee PSC beams.

Alternative II, utilizes is a two span bridge (65 ft each), that consists of AASHTO type II beams. This span arrangement requires a middle bent, in the main channel of Camp Creek.

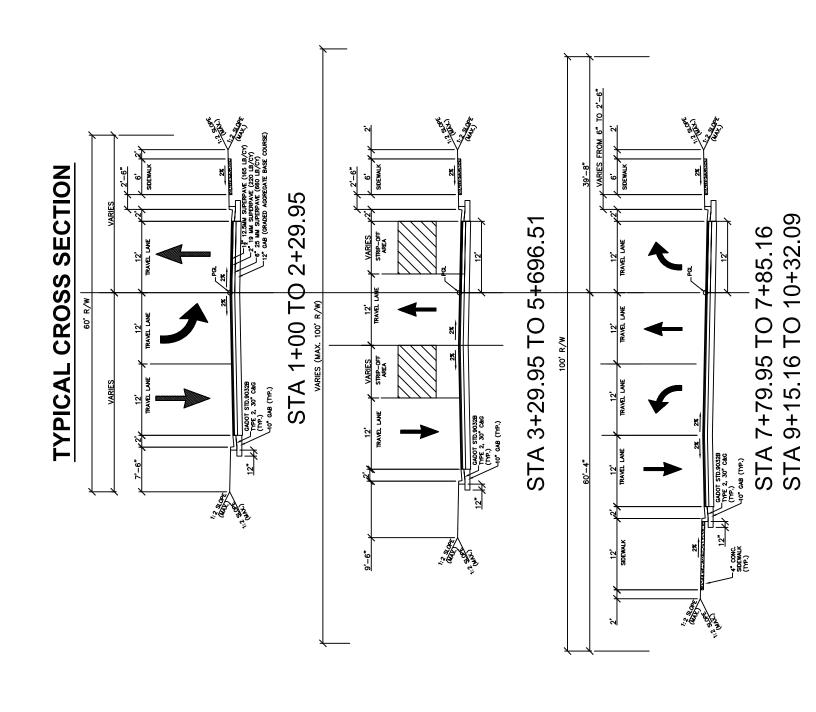
Alternative III consists of a single, 130-ft long span structure, made of 65" bulb-tee PSC beams.

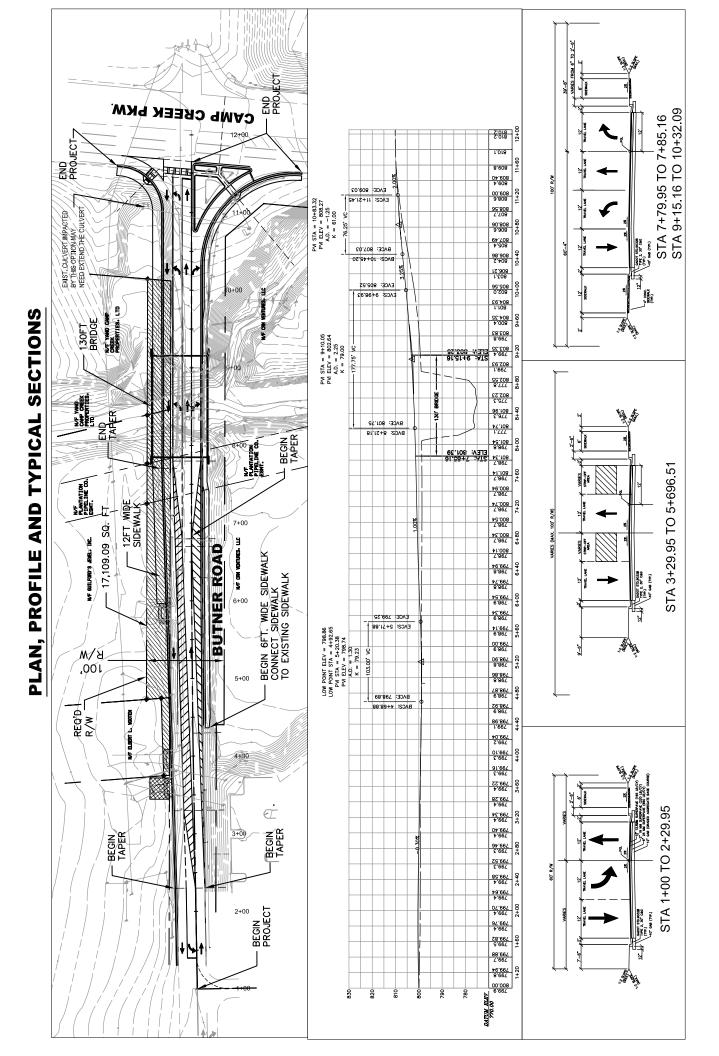
Georgia DOT design criteria require that, for this type of road, the proposed bridge provide a minimum of 2.0 ft of clearance above the design-year storm floodstage, and a minimum of 0.5 ft of clearance above the 100-year storm floodstage. The design-year storm in this case is the 50-year storm event.

Based on the results from simulations of the proposed conditions, Alternative III meets this criterion. Also, the backwater values, which are calculated by measuring the effect of the existing and the proposed encroachment on the floodplain over the natural conditions, have to be considered in the design of the proposed bridge.

Georgia DOT design criteria require that the backwater be less than 1.0 ft. Alternative III meets this criterion too.

Hydraulically, the other two alternatives do not work as well as Alternative III, taking into account the width of the main channel.





### **Estimate Report for file "Butner Road -2010-05-27"**

Item Number	Quantity	Units	<b>Unit Price</b>	Item Description	Cost
150-1000	1	LS	20000.0	TRAFFIC CONTROL -	20000.0
153-1300	1	EA	40750.0	FIELD ENGINEERS OFFICE & Mobilization	40750.0
201-1500	1	LS	50000.0	CLEARING & GRUBBING -	50000.0
210-0100	1	LS	705000.0	GRADING COMPLETE -	705000.0
310-5100	3300	SY	16.44	GR AGGR BASE CRS, 12 INCH, INCL MATL	54252.00
402-1812	60	TN	69.41	RECYCLED ASPH CONC LEVELING, INCL BITUM MATL & H LIME	4164.59
402-3121	257	TN	59.9	RECYCLED ASPH CONC 25 MM SUPERPAVE, GP 1 OR 2, INCL BITUM MATL & H LIME	15394.3
402-3130	20	TN	64.18	RECYCLED ASPH CONC 12.5 MM SUPERPAVE, GP 2 ONLY, INCL BITUM MATL & H LIME	1283.60
402-3190	30	TN	67.17	RECYCLED ASPH CONC 19 MM SUPERPAVE, GP 1 OR 2,INCL BITUM MATL & H LIME	2015.10
413-1000	200	GL	2.13	BITUM TACK COAT	426.0
432-0208	1300	SY	5.64	MILL ASPH CONC PVMT, 2 IN DEPTH	7332.0
441-0016	35	SY	41.13	DRIVEWAY CONCRETE, 6 IN TK	1439.55
441-0104	1023	SY	32.82	CONC SIDEWALK, 4 IN	33574.86
441-6012	1823	LF	16.09	CONC CURB & GUTTER, 6 IN X 24 IN, TP 2	29332.07
550-1240	400	LF	46.58	STORM DRAIN PIPE, 24 IN, H 1-10	18632.0
550-4224	2	EA	744.82	FLARED END SECTION 24 IN, STORM DRAIN	1489.64
603-2182	2	SY	53.72	STN DUMPED RIP RAP, TP 3, 24 IN	107.44
610-1055	600	LF	2.11	REM GUARDRAIL	1266.0
610-1075	4	EA	160.89	REM GUARDRAIL ANCH, ALL TYPES	643.56
641-1200	916	LF	17.6	GUARDRAIL, TP W	16121.60
641-5005	4	EA	1008.31	GUARDRAIL ANCHORAGE, TP 5	4033.24
668-1100	4	EA	2541.9	CATCH BASIN, GP 1	10167.6
668-4300	2	EA	2250.04	STORM SEWER MANHOLE, TP 1	4500.08

<b>Section Signing</b>	Section Signing and Marking										
Item Number	Quantity	Units	Unit Price	Item Description	Cost						
611-5551	12	EA	368.24	RESET SIGN	4418.88						
634-1200	12	EA	99.08	RIGHT OF WAY MARKERS	1188.96						
652-5301	2400	LF	0.15	SOLID TRAF STRIPE, 6 IN, WHITE	360.0						
652-5452	2400	LF	0.21	SOLID TRAFFIC STRIPE, 5 IN, YELLOW	504.0						
652-5701	14	LF	2.1	SOLID TRAF STRIPE, 24 IN, WHITE	29.40						
653-0300	14	EA	200.0	THERMOPLASTIC PVMT MARKING, SYMBOL, TP 1	2800.0						
654-1001	70	EA	3.06	RAISED PVMT MARKERS TP 1	214.20						
				Section Sub Total:	\$9,515.44						

<b>Section Erosion</b>	Section Erosion Control Items										
Item Number	Quantity	Units	Unit Price	Item Description	Cost						
163-0232	1	AC	385.22	TEMPORARY GRASSING	385.22						
163-0240	5	TN	172.38	MULCH	861.9						
163-0300	2	EA	1234.88	CONSTRUCTION EXIT	2469.76						
163-0524	4	EA	183.88	CONSTRUCT AND REMOVE TEMPORARY DITCH CHECKS - STONE PLAIN RIP RAP/SAND BAGS	735.52						
163-0531	2	EA	10913.09	CONSTRUCT AND REMOVE SEDIMENT BASIN, TP 1, STA NO -	21826.18						
165-0030	1400	LF	0.78	MAINTENANCE OF TEMPORARY SILT FENCE, TP C	1092.0						
165-0040	24	EA	57.2	MAINTENANCE OF EROSION CONTROL CHECKDAMS/DITCH CHECKS	1372.80						
165-0041	240	LF	1.94	MAINTENANCE OF CHECK DAMS - ALL TYPES	465.59						
167-1000	10	EA	597.96	WATER QUALITY MONITORING AND SAMPLING	5979.6						
171-0030	1400	LF	3.46	TEMPORARY SILT FENCE, TYPE C	4844.0						
700-6910	2	AC	825.66	PERMANENT GRASSING	1651.32						
700-7000	3	TN	63.09	AGRICULTURAL LIME	189.27						
700-7010	6	GL	21.49	LIQUID LIME	128.94						
700-8000	1	TN	384.56	FERTILIZER MIXED GRADE	384.56						
700-8100	50	LB	2.3	FERTILIZER NITROGEN CONTENT	114.99						
716-2000	2500	SY	0.96	EROSION CONTROL MATS, SLOPES	2400.0						
				Section Sub Total:	\$44,901.67						

Total Estimated Cost: \$1,076,342.35

Subtotal Construction Cost \$1,076,342.35

E&C Rate 10.0 % \$107,634.23

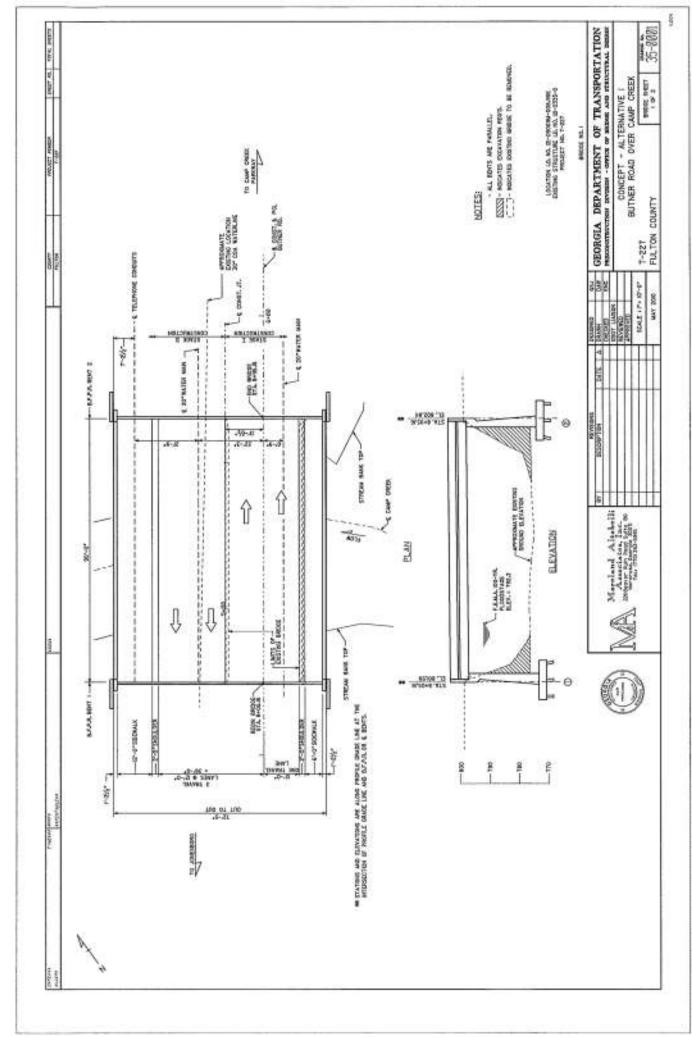
Inflation Rate 2.0 % @ 1 Years \$23,679.53

Total Construction Cost \$1,207,656.12

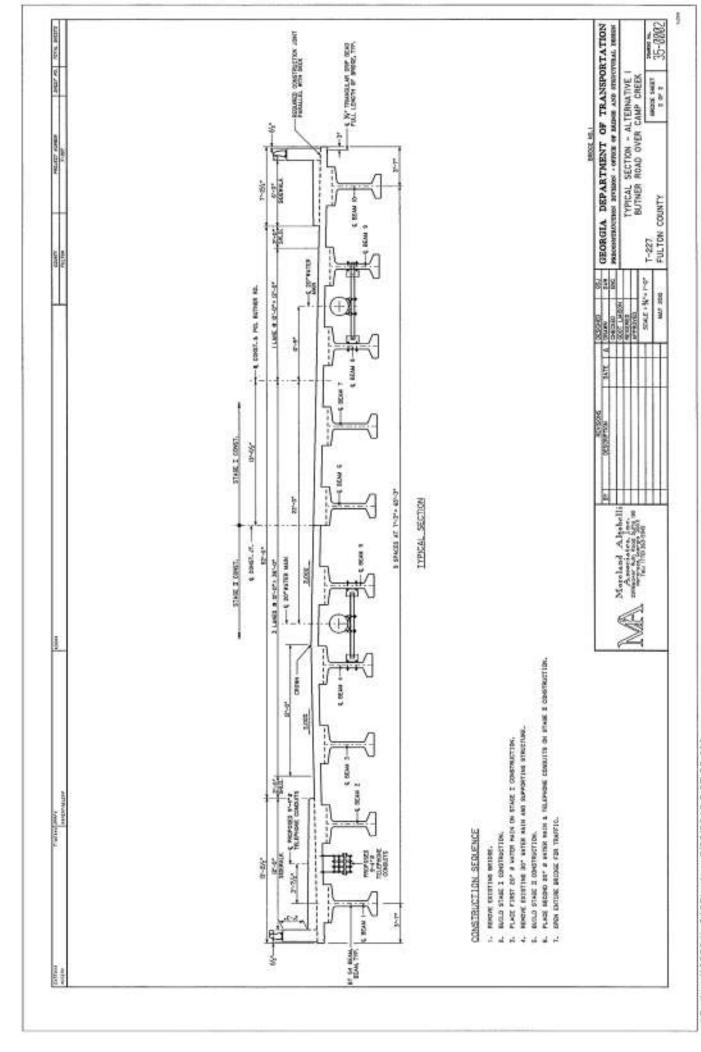
Right Of Way 40000.00

ReImb. Utilities 0.00

Grand Total Project Cost \$1,247,656.12



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### Cost Estimate Alternative 1 1 Span

Project: 08504 Project Number:

Made By:

Checked By:

Butner Road Over Camp Creek

T227 QSJ

Date: 25-May-10

Date:

	BT-54/AI	but Walls						
Tag	Pay Item	Description	Quantity	Unit	L	Jnit Cost		Cos
170	500-0100	GROOVED CONCRETE	833	SY	s	4.67	\$	3,891.6
171	500-1006	SUPERSTR CONCRETE, CL AA, BR NO -	218	LS	S	762,56	\$	186,125.6
187	500-3800	CLASS A CONCRETE, INCL REINF STEEL	614	CY	\$	628.37	\$	385,819.1
198	507-9030	PSC BEAMS, AASHTO, BULB TEE, 54 IN, BR NO -	900	LF	s	162.30	s	146,070.0
						, , , , , , , , , , , , , , , , , , ,		
202	511-1000	BAR REINF STEEL		LB	s	88.0		
203	511-3000	SUPERSTR REINF STEEL, BR NO -	59256	LS	\$	0.92		54,515.4
207	516-1100	ALUM HANDRAIL, STD 3626	180	LF	\$	54.15		9,747.0
218	520-1147	PILING IN PLACE, STEEL H, HP 14 X 73	720	LF	\$	72.18	\$	51,969.6
250	522-1000	SHORING	1	LS	s	121,892.50	\$	121,892.5
253	520-1320	COFFERDAM	2	EA	\$	14,361.48		28,722.9
259	540-1101	REMOVAL OF EXISTING BR, STA NO -	1	LS	\$	115,792.88	\$	115,792.8
350	603-2024	STN DUMPED RIP RAP, TP 1, 24 IN	468	SY	8	48.24	\$	22,587.3
355	603-7000	PLASTIC FILTER FABRIC	468	SY	3	4.42		2,069.5
432	627-1020	MSE WALL FACE, 20 - 30 FT HT, WALL NO -	4000	SF	\$	56.00	\$	224,000.0
			.22 700 700 00 00 00 00 00		0.000	Sub Total =		1,333,203.7
			Deck Area Per					6,517.5
				Unit	Cost	(\$ / sq ft) =	\$	204.5

Total Bridge Cost = \$ 1,493,187.78

\$

\$

\$

66,660.00

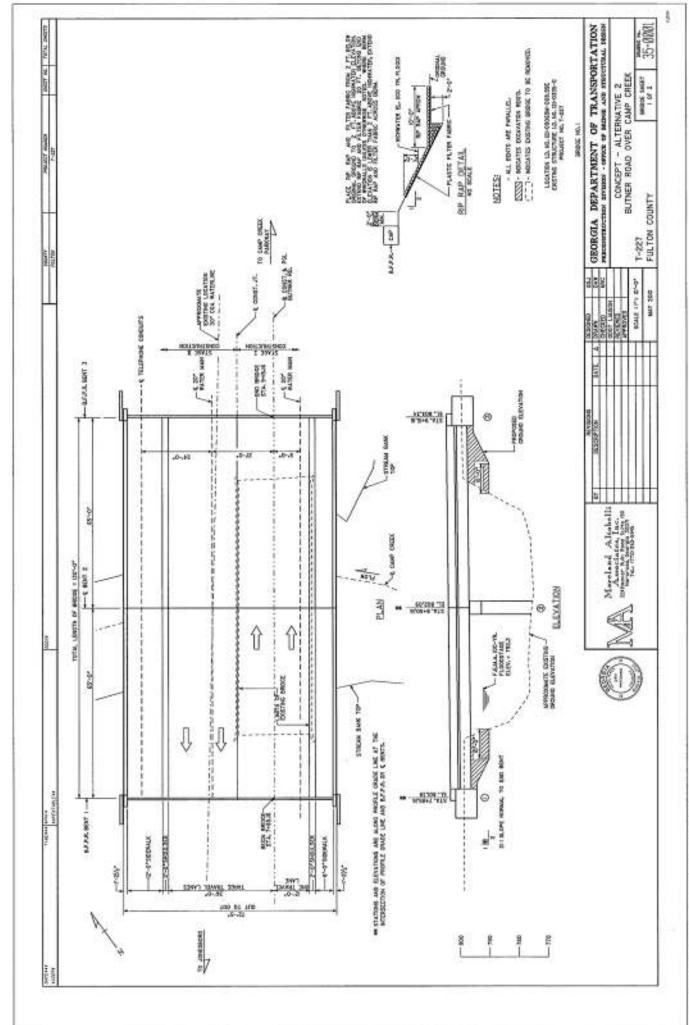
66,660.00

26,664.00

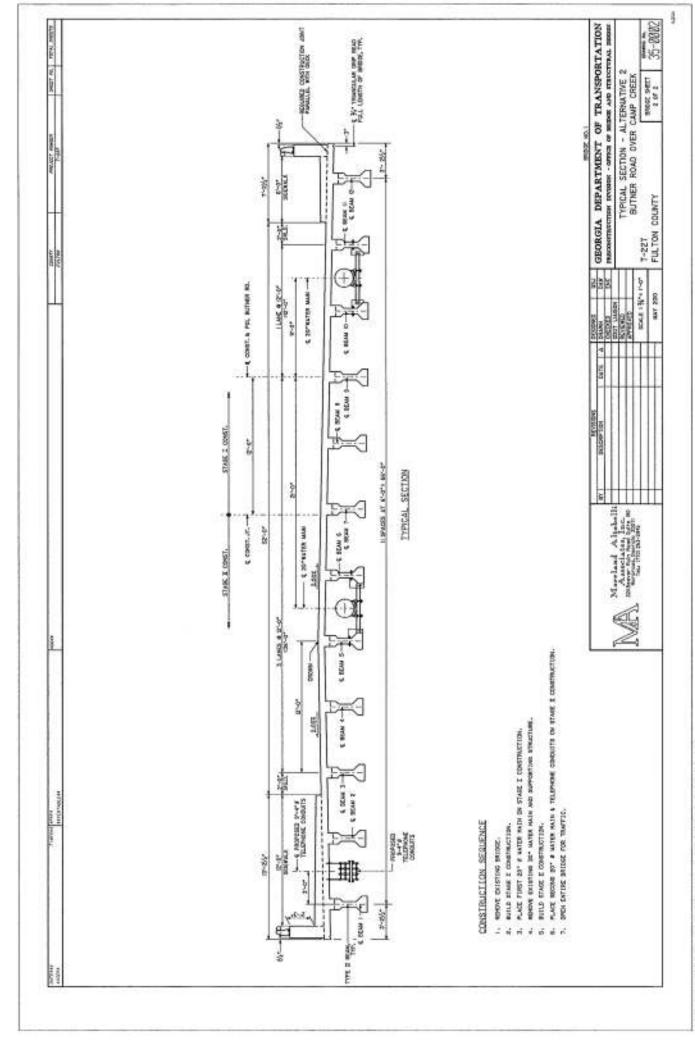
5% Mobilization

2% Contigency

5% MOT



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**Cost Estimate** Alternative 2 2 Spans TP II/Endrolls

Checked By:

Project: 08504

Butner Road Over Camp Creek

Project Number: T227

Made By: QSJ

Date: 25-May-10

Date:

Tag	Pay Item	Description	Quantity	Unit	U	nit Cost	_	Cost
65	211-0300	BRIDGE EXCAVATION, STREAM CROSSING	38	CY	\$	29.59	\$	1,134.28
170	500-0100	GROOVED CONCRETE	1056	SY	3	4.67	3	4,929.44
171	500-1006	SUPERSTR CONCRETE, CL AA, BR NO -	282	LS	3		S	215,054.02
176	500-3002	CLASS AA CONCRETE	210	CY	\$	488.44	\$	102,409.59
195	507-9002	PSC BEAMS, AASHTO TYPE II, BR NO -	1560	LF	\$	124.69	\$	194,516.40
					1100			
202	511-1000	BAR REINF STEEL	30821	LB	\$	88.0	\$	27,122.48
203	511-3000	SUPERSTR REINF STEEL, BR NO -	76708	LS	\$	0.92		70,571.65
207	516-1100	ALUM HANDRAIL, STD 3626	260	LF	\$	54.15		14,079.00
218	520-1147	PILING IN PLACE, STEEL H, HP 14 X 73	1440	LF	\$	72.18	\$	103,939.20
250	522-1000	SHORING	1	LS	\$ 1	121,892.50	\$	121,892.50
253	520-1320	COFFERDAM	3	EA		14,361.48		43,084.44
259	540-1101	REMOVAL OF EXISTING BR, STA NO -	1	LS	\$	115,792.88	\$	115,792.88
350	603-2024	STN DUMPED RIP RAP, TP 1, 24 IN	468	SY	\$	48.24	\$	22,587.37
355	603-7000	PLASTIC FILTER FABRIC	468	SY	\$	4.42	\$	2,069.57
432	627-1020	MSE WALL FACE, 20 - 30 FT HT, WALL NO -	4000	SF	\$	44.37	\$	177,480.00
				D-I	dan C	ub Total =		1,216,662.82
			Deck Area Per					9,414.17
			Deck Area Pe		TO OTHER DESIGNATION OF THE PERSON OF THE PE	\$ / sq ft) =		129.24
		5% Mobilization					\$	60,833.00

Total Bridge Cost = \$ 1,362,661.82

\$

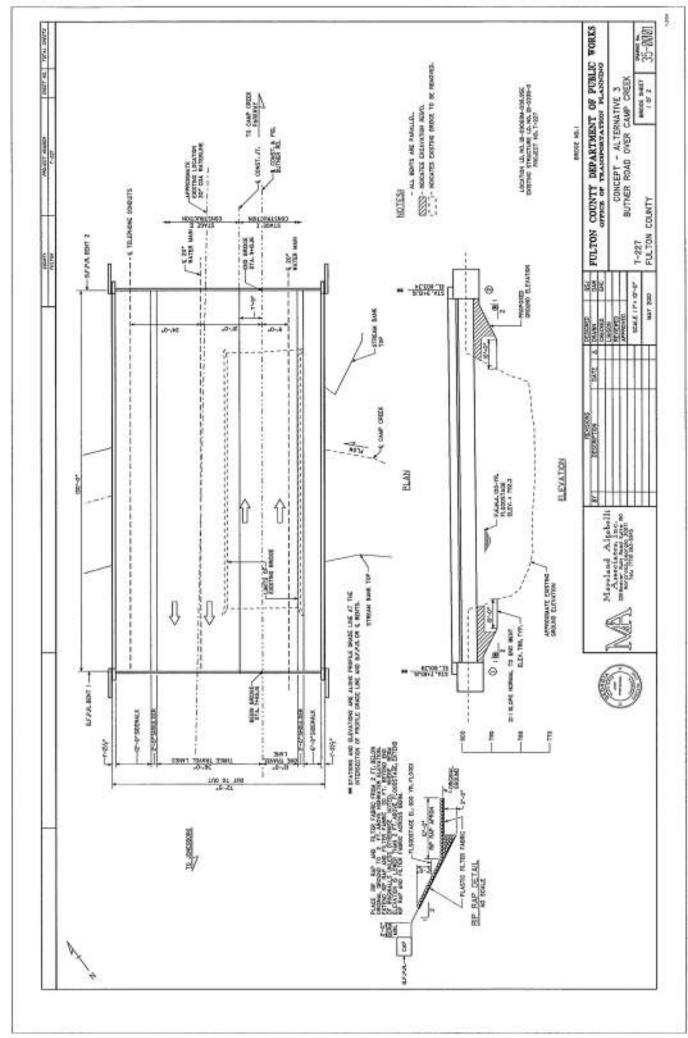
\$

60,833.00

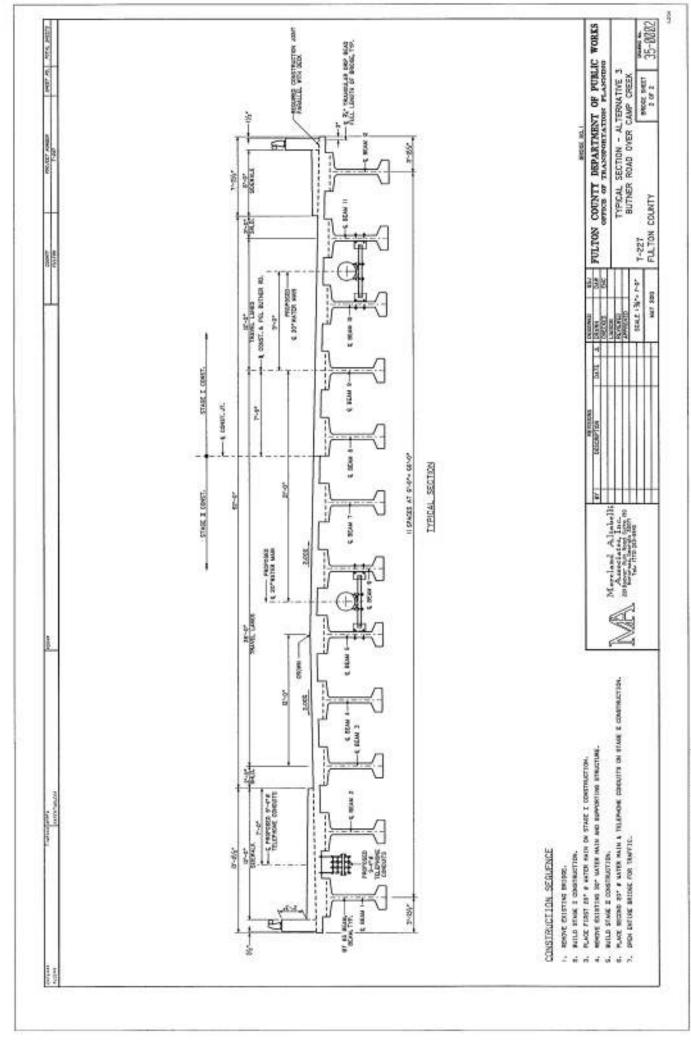
24,333.00

5% MOT

2% Contigency



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### **Cost Estimate** Alternative 3 1 Span BT-65/ENDROLLS

Project: 08504

Butner Road Over Camp Creek

Project Number : T227

Made By: QSJ Checked By:

Date: 25-May-10

Date:

Co		Init Cost	U	Unit	Quantity	Description	Pay Item	Tag
4,929.4	8	4,67	\$	SY	1056	GROOVED CONCRETE	500-0100	170
227,673.9		762.56	\$	LS	299	SUPERSTR CONCRETE, CL AA, BR NO -	500-1006	171
9,046.7	s	246.73	\$	CY	37	CLASS A CONCRETE	77 500-3101 CLASS A CC	177
400-100-70				otest	Sylvano		the Market Co.	25.5
289,302.0	S	185.45	\$	LF	1560	PSC BEAMS, AASHTO, BULB TEE, 63 IN, BR NO -	507-9031	199
4,743.2	s	0.88	\$	LB	5390	BAR REINF STEEL	511-1000	202
74,712.9		0.92	\$	LS	81210	SUPERSTR REINF STEEL, BR NO -	511-3000	203
14,079.0	CAAC	54.15	S	LF	260	ALUM HANDRAIL, STD 3626	516-1100	207
51,969.6	\$	72.18	s	LF	720	PILING IN PLACE, STEEL H, HP 14 X 73	520-1147	218
121,892.5	\$	121,892.50	\$ 1	LS	1	SHORING	522-1000	250
115,792.8	\$	115,792.88	\$ 1	LS	.1	REMOVAL OF EXISTING BR, STA NO -	540-1101	259
22,587.3	\$	48.24	s	SY	468	STN DUMPED RIP RAP, TP 1, 24 IN	603-2024	350
2,069.5		4.42	S	SY	468	PLASTIC FILTER FABRIC	603-7000	355
177,480.0	\$	44.37	s	SF	4000	MSE WALL FACE, 20 - 30 FT HT, WALL NO -	627-1020	432
1,116,279.2	\$	ub Total =	dae S	Bri				
9,414.1	\$	BL (BW) =	ft) =	Side (so	Deck Area Per			
118.5	\$	(\$ / sq ft) =	Cost (	Unit				
55,814.0	\$					5% Mobilization		
55,814.0	\$					5% MOT	The state of the s	
22,326.0	\$					2% Contigency		

Total Bridge Cost = \$ 1,250,233.27

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25-May-10

Date :

T227

08504 QSJ

Project : Project Number : Made By : Checked By:

Butner Road Over Camp Creek

		200
BR No.	Bridge Description	Estimated Cost
-	Alternative 1, 90 Feet Single Span Bridge with Abutments	\$ 1,493,187.78
-	Alternative 2, 130 Feet Bridge with Two 65 Feet Spans and End Rolls	\$ 1,362,661.60
-	Alternative 3, 130 Feet Single Span Bridge with End Rolls	\$ 1,250,233.27

Total Bridge Sq FT= 9414 Price/Sq FT= \$ 118.57

## PREFERRED ALTERNATIVE IS #3

# BRIDGE INVENTORY DATA LISTING GEORGIA DEPARTMENT OF TRANSPORTATION

Location & Geography						Signs &	Signs & Attachments	
- Structure LD No.	121-0355-0			104 Highway System:	0	200	Exmansion Joint Type:	0.5
200 Bridge Information	07			26 Functional Classification:		Name of		
* 6A Feature Int:	CAMP CREEK		*	204 Federal Route Type:	M No.: 09069	242	Deck Drams;	
<ul> <li>648 Critical Bridge:</li> </ul>	o		=	105 Federal Lands Highway:	0	243	Parapet Location:	0
<ul> <li>7A Route Number Carried:</li> </ul>	CR01374			110 Truck Route:	0		Height	0.00
* 7B Encility Carried:	BUTNER ROAD		n	206 School Bus Route:	-		Width	0.00
* 9 Location:	5.8 MI W OF COLLEGE PARK		rı	217 Benchmark Elevation:	0000000			
2 DOT District:	7		-	218 Datum:	0	238	Curb:	1.000.1
207 Year Photo:	6661				90	239	Handrailt	5
* 91 Inspection Frequency:	24 Date: 10/20/2004			20 Tolk	3	* 240	Median Barrior Rail:	0
92A Fract Crit Insp Freat				21 Maintenance:	0.5			0.00000
9213 Underwater lasp Fred:	9			22 Owner.	02	241	Bridge Median Height:	0.460
92C Other Soc. Insp Freq:	00			31 Design Load:	2		Width:	0.00
* 4 Place Code:	ĕ			37 Historical Significance:	\$			•
* 4 Inventory Route (OVI):			71	205 Congressional District:	05	. 230	Guardina Loc Dir	23266
Tomes	- 4				1946		Fwrd;	3 0 1327
Designation:			-		0000		Oppo Dir Rear.	577 0
Number	69060			33 Bridge Median:			Fwnd:	0
Direction	0			34 Skew;	00	244	Approach Slab:	0
* 16 Lutitude: 33-40.1	MMS Prefix: 00			35 Structure Planed:	0	224	Retaining Wall	-
* 17 Lanaitude: 84-37 8	MMS Suffix: 000 MP: 0	0.00		38 Navigation Control:				
no Brasles Bull no	3		-	211 Special Steel Design:	0		Posted Speed Limit:	7
98 contact condice				4		236	Warning Sign:	0
99 ID Namber:	(1)0100100100100100			Type o	21.	234	Delineator:	0
* 100 STRAHNET:	0			42 Type of Service on:	V	235	Hazard Boards:	0
12 Base Highway Network:	1		-			21.0		00
13A LRS Inventory Route:	1212137400		4.5	-0	TOWO		Offilias Off	F
13B Sub Inventory Route:	0		4 5	200 13pt trings.			* 1	ī :
* 101 Perellal Structure	Z						Elle	00
TALL PRODUCT COURSE.					3 42		Telephone:	22
102 Direction of Traffic:					1003		35	00
<ul> <li>264 Road Inventory Mile Post:</li> </ul>	bst: 009.15			44 Structure Type Appr:	00 0			
* 208 Inspection Area:	69 Initials: JMC			46 No. Spans Appr.		247	Lighting Street:	0
Frankowsky Initial			-	226 Bridge Curve Horz:	0 Vent: 0		Navingtion:	0
The state of the s				111 Pier Protection:	0		Aerial:	0
				107 Deck Structure Type:				
* Location LD. No.: 12	121-09069M-008.95E		_	108 Wearing Surface Type: Me	90	* 248	<ul> <li>248 County Continuity No.:</li> </ul>	00

# BRIDGE INVENTORY DATA LISTING GEORGIA DEPARTMENT OF TRANSPORTATION

Mrucine ID: 121-0222-0			
Programming Data		Measurements	Ratings
		100000000000000000000000000000000000000	65 Inventory Rating Method:
	NMC	(102650 Y car.	63 Januardon Patina Method:
202 Plans Available:	0	109 % Trucks: 0	25 Illychiaily hearing continues
249 Prop. Proj. No.	0000000000000000	<ul> <li>28 Lanes On: 02 Under: 00</li> </ul>	Gunda 7
250 Approval Status:	0000	On Under	64 Operating Type: 2 Kating:
	0000000	ode. 00036	231 Calculated Loads
	1001/1001		H-Modified: 11
	000000		H&Modified: 17 0
260 Seismic No.:	nonon	51 Br. Rwdy, Width: 24.00	The Same
75 Type Work:	31 1	52 Deck Widtle 29.00	
94 Bridge Imp. Cost:	\$ 143	* 47 Tot. Horz, Cl: 24.00	
95 Roadway Imp. Cost:	\$ 337	Width: 1.00	Tumber: 20
96 Total Imp Cost:	\$ 546	÷	夏
	001410	W IOIII.	261 H Inventory Rating: 10
97 Inn Year	1990	229 Shoulder Width:	262 H Operating Rating: 17
AND STREET WANTED	0000074 Venne 2024	5.00 lype: 8 Rt:	
114 raime vist.		Fwed Lat. 1.50 Type: 1 KE 1.50	
		Pavement Widin;	59 Superstructure Condition: 6
		24 00 Tunner	* 227 Collision Damage: 0
		Lanconstant Brees 0 Freed	60A Substructure Condition: 4
Hardwardte Date			60B Scour Condition: 8
Hydraune Data			60C Underwater Condition: 5
215 Waterway Data			A CONTRACTOR OF THE PARTY OF TH
Highwaler Elev.	0000.0 Year, 1900		
A con Streamshord Clear	0.0000	0	on Cond.
AVE. Strenming Law	nonon	33	68 Deck Geometry: 2
Dramage Area.	000000	Under: N 00 ' 00 "	69 UnderClr, Horz/Vert: N
Area Or Opening.	11	* 228 Min Vertical Ci	72 Appr. Alignment: 8
113 Sonar Childia			62 Culvert; N
216 Water Depth:	01.0 Br. magns: 22.0	ALC:	
222 Slope Protection:			Posting Data
221 Spur Diloes Rear.	0 Fwrd: 0	, Dir.	
219 Fender System:	0	Oppo. Dir. 00 * 00 *	
220 Dolphin:	0	55 Lateral Uniberel, Rt: N 99,90	
223 Culvert Cover	000	56 Lateral Underel, Lt. 0.00	=
	0	100	232 Posted Louds 11-Modified: 11
No. Barrels:	0	20 21 22 22	HS-Modified: 00
	0.00 Neight: 0.90	Nav Vert CE MIN FROM:	Type 3: 14
Longth: 0	Apron: 0	Nav Vert Cl Closed: 000	Type3s2: 00
* 265 U/W losm Area:	1 Diver: RM	245 Deck Thickness Main: 7.00	Timber: 20
		Dock Thick Approach:	Piggyback: 00
		25	253 Notification Date 02/01/1901
* Toesting D Nov. 15	THE WOOLDS AND COLD	All Vine I am Baladadh Same 2004 Stabe (1900)	

